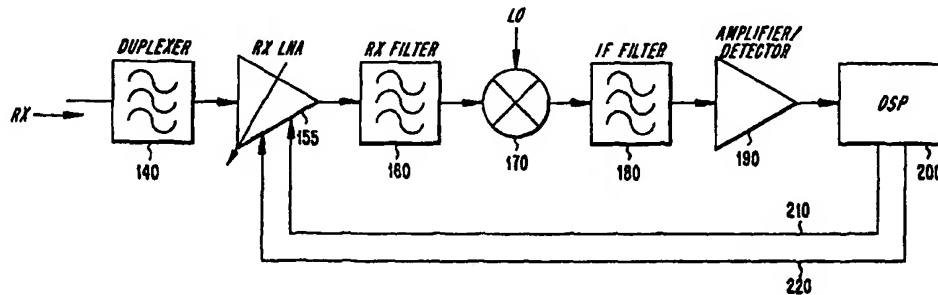


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<b>(21) International Application Number:</b> PCT/US99/04783  <b>(22) International Filing Date:</b> 4 March 1999 (04.03.99)  <b>(30) Priority Data:</b> 09/035,944      6 March 1998 (06.03.98)      US  <b>(71) Applicant:</b> ERICSSON INC. [US/US]; 7001 Development Drive, Research Triangle Park, NC 27709 (US).  <b>(72) Inventor:</b> FREED, John, G.; 8909 Lindenshire Road, Raleigh, NC 27615 (US).  <b>(74) Agents:</b> GRUDZIECKI, Ronald, L. et al.; Burns, Doane, Swecker & Mathis, L.L.P., P.O. Box 1404, Alexandria, VA 22313-1404 (US).	<b>(81) Designated States:</b> AL, AM, AT, AU, AZ, BA, BB, BG, BR, BY, CA, CH, CN, CU, CZ, DE, DK, EE, ES, FI, GB, GD, GE, GH, GM, HR, HU, ID, IL, IN, IS, JP, KE, KG, KP, KR, KZ, LC, LK, LR, LS, LT, LU, LV, MD, MG, MK, MN, MW, MX, NO, NZ, PL, PT, RO, RU, SD, SE, SG, SI, SK, SL, TJ, TM, TR, TT, UA, UG, UZ, VN, YU, ZW, ARIPO patent (GH, GM, KE, LS, MW, SD, SL, SZ, UG, ZW), Eurasian patent (AM, AZ, BY, KG, KZ, MD, RU, TJ, TM), European patent (AT, BE, CH, CY, DE, DK, ES, FI, FR, GB, GR, IE, IT, LU, MC, NL, PT, SE), OAPI patent (BF, BJ, CF, CG, CI, CM, GA, GN, GW, ML, MR, NE, SN, TD, TG).  <b>Published</b> <i>With international search report.</i> <i>Before the expiration of the time limit for amending the claims and to be republished in the event of the receipt of amendments.</i>	

**(54) Title:** APPARATUS, SYSTEM, AND METHOD FOR IMPROVING THE DYNAMIC RANGE OF A RECEIVER IN THE PRESENCE OF A NARROWBAND INTERFERING SIGNAL

**(57) Abstract**

An apparatus, system and method improve the dynamic range of a receiver in the presence of a narrowband interfering signal. An error rate of a received signal is computed, and the input intercept point of a low noise amplifier in the receiver is adjusted based on the error rate. The transmit power level is detected, and the input intercept point is adjusted based also on the transmit power level. The received signal strength is also detected, and the gain of the low noise amplifier is adjusted based on the received signal strength. In this manner, the effect of crossmodulation on the received signal is reduced.

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**APPARATUS, SYSTEM, AND METHOD FOR IMPROVING THE DYNAMIC  
RANGE OF A RECEIVER IN THE PRESENCE OF  
A NARROWBAND INTERFERING SIGNAL**

5 **BACKGROUND**

This invention relates to an apparatus, system, and method for improving the dynamic range of a receiver. More particularly, this invention relates to an apparatus, system, and method for improving the dynamic range of a receiver in the presence of a narrowband interfering signal.

10 Duplex radio systems, such as a Code Division Multiple Access (CDMA) duplex radio system, use spread spectrum full duplex transmission to transmit and receive cellular telephone calls. In a CDMA radio system according to the IS-95 standard, information to be transmitted is typically digitized, encoded, and spread over a 1.23 Mega Hertz (MHz) bandwidth. A typical IS-95 subscriber unit transmitter uses Offset  
15 Quadrature Phase Shift Keying (OQPSK) modulation which contains both time varying phase and amplitude components. Thus, the transmitter output has an amplitude modulation (AM) component and is not a constant envelope signal. A CDMA base station uses Quadrature Phase Shift Keying (QPSK) modulation with both time-varying phase and amplitude components. At the receiving end, the wideband spread signal is  
20 despread, decoded, and converted back into analog form. Frequency selective filters, referred to as duplexors, are used in the subscriber unit to combine the transmit and receive signals together to permit simultaneous transmit and receiver operation.

FIG. 1 illustrates a conventional subscriber unit duplex system. The system includes a transmit (TX) path and a receive (RX) path. The TX path includes a Driver  
25 110 for amplifying an OQPSK modulated signal, a TX Filter 120 for filtering the modulated signal, and a Power Amplifier (PA) 130 for amplifying the filtered signal for transmission. The signal is filtered by a Duplexor 140 and transmitted to a base station via an Antenna 145. A signal is received from the base station via the Antenna 145 and filtered by the Duplexor 140. Because the Duplexor isolation is not infinite, a portion,

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$P_{TX-RX}$ , of the transmit signal appears at the receiver input when the transmitter is turned on. The received signal is amplified by an RX Low Noise Amplifier (LNA) 150, filtered by an RX Filter 160, and mixed with a local oscillator (LO) frequency in a Mixer 170. The received signal is then fed, for example, to an IF filter.

5           As CDMA systems are deployed into systems using the current Advanced Mobile Phone System (AMPS) cellular telephone band, a potential source of interference exists between the wideband spread spectrum signal transmitted by an IS-95 subscriber unit and the relatively narrowband AMPS signal coexisting in the same frequency band. If an AMPS signal, or any narrowband signal, is present within the RF passband of the  
10 receiver when the transmitter is on, the AM component of the transmit signal is transferred onto the narrowband signal, due to third order nonlinearity in the LNA 150. This effect, which is referred to as crossmodulation, is well known in amplitude modulation systems.

          Because the bandwidth of a CDMA transmit signal is relatively large (1.23 MHz),  
15 it is possible for this wideband TX crossmodulation signal to appear in the IF passband of the desired receive signal, depending on where the narrowband interfering signal is located with respect to the desired RX channel. In fact, for any narrowband interfering signal having a center frequency closer to the RX center frequency than the TX spread bandwidth plus half the RX channel bandwidth, the TX crossmodulation product falls in  
20 the IF bandwidth. In an AMPS/CDMA system, this means that any narrowband interfering signal having a center frequency within approximately 1.85 MHz of the RX center frequency creates undesired TX modulation within the RX IF passband. The net effect of this crossmodulation product is to mask the desired receive signal, thus reducing the sensitivity of the receiver. This effect is illustrated in FIGS. 2A and 2B.

25           FIG. 2A illustrates a TX modulated signal. FIG. 2B illustrates the TX modulated signal transferred onto a narrowband interfering signal. As can be seen from the shading in FIG. 2B, the TX crossmodulation falls within the desired RX bandwidth, masking the desired receive signal and reducing the dynamic range of the receiver by effectively increasing the noise floor of the receiver.

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This effect can also occur in the Mixer 170 illustrated in FIG. 1. However, the attenuation of the RX Filter 160 and the Mixer 170's third order input intercept point can be selected to suppress the TX signal enough so that the Mixer 170 does not contribute any appreciable additional crossmodulation product.

5       The level of TX modulation appearing about the narrowband interfering signal varies linearly with the level of the narrowband interfering signal and the modulation index of the TX modulation (% modulation), the square of the amplitude of the TX signal appearing at the LNA input ( $P_{TX-RX}$  in FIG. 1), and inversely as the square of the third order input intercept point of the LNA 150. Thus, the factors that contribute to the crossmodulation product are the amplitudes of the TX signal and the narrowband  
10       interfering signal, the modulation index of the TX signal, and the third order input intercept point of the LNA 150.

Of the factors contributing to the generation of the undesired crossmodulation products, the modulation index is fixed by the system and cannot be changed. The  
15       amplitude of the TX signal appearing at the LNA input can be reduced by specifying more TX-RX attenuation in the Duplexor 140. However, in a small subscriber unit, the practical limit of isolation that can be achieved is not sufficient to eliminate the generation of the crossmodulation product. It is also not practical to reduce the amplitude of the narrowband interfering signal appearing in the RX band, since any attempt to do so  
20       would also reduce the level of the desired RX signal.

Conventionally, the third order input intercept point of the LNA 150 is varied to minimize the generation of crossmodulation products. An example of an LNA with a variable third order input intercept point is the RF 9986 integrated circuit produced by RF Micro-Devices. Conventionally, the third order input intercept point of the LNA is set at  
25       a maximum level while the transmitter operates at relatively high power and then switched to a minimum level while the transmitter operates at reduced power. This improves the dynamic range of the receiver to some extent and also saves current, since the lower third order input intercept point generally requires less current from the power supply. In addition to controlling the third order input intercept point of the LNA, the

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gain of the LNA is typically also reduced under strong on-channel signal conditions to help improve receiver dynamic range.

While the conventional approach is effective for many situations, it does not provide adequate dynamic range of the receiver in at least one situation, e.g., when the subscriber unit is operating relatively close to a base station and a narrowband signal appears. In this situation, the subscriber unit transmitter is operating at reduced power, and the LNA's third order input intercept point, which is adjusted depending on the transmit power level, is set at the minimum level. If a strong AMPS signal or other narrowband signal, originating from an AMPS base station co-located with the CDMA base station, an AMPS microcell within the larger CDMA cell, or another source, appears within the  $\pm 1.85$  MHz region around the subscriber unit's RX channel, the strong narrowband interfering signal mixes with the subscriber unit TX signal and generates on-channel crossmodulation products. This causes a reduction in RX signal-to-noise ratio and possibly a loss of communications.

Linking the control of the LNA's third order input intercept point to the transmit power level is thus, not alone, sufficient to achieve the optimum dynamic range to deal with narrowband interfering signals that are likely to be encountered in actual system operation.

There is thus a need for method and system for increasing the dynamic range of a receiver in the presence of a narrowband interfering signal which overcomes the drawbacks of the prior art.

## SUMMARY

It is therefore an object of the invention to provide an apparatus, system, and method for increasing the dynamic range of a receiver in the presence of a narrowband interfering signal.

According to an exemplary embodiment, an error rate of a received signal is computed, and the input intercept point of a low noise amplifier in the receiver is adjusted based on the error rate. The transmit power level is detected, and the input

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intercept point is adjusted based also on the transmit power level. If the transmit power level is low, and the computed error rate exceeds a predetermined threshold, the input intercept point is set at a maximum level. If the transmit power level is low, and the computed error rate does not exceed a predetermined threshold, the input intercept point is set at a minimum level. If the transmit power level is high, the input intercept point is set at a maximum level. The received signal strength is also detected, and the gain of the low noise amplifier is adjusted based on the received signal strength.

### BRIEF DESCRIPTION OF THE DRAWINGS

Exemplary embodiments of the invention will now be described in more detail with reference to the accompanying drawings, in which like descriptive labels are used to refer to similar elements and in which:

FIG. 1 illustrates a conventional subscriber unit duplex system;

FIG. 2 illustrates a problem with the conventional duplex system;

FIG. 3 illustrates a receiver path according to an exemplary embodiment of the present invention;

FIG. 4 illustrates a method according to an exemplary embodiment of the present invention; and

FIGS. 5A-5D illustrate simulations according to an exemplary embodiment of the present invention.

### DETAILED DESCRIPTION

In this description, specific details such as particular circuits, circuit components, techniques, etc., are set forth for purposes of explanation and not limitation in order to provide a thorough understanding of the invention. It will be apparent to one of ordinary skill in the art that the invention may be practiced in other embodiments that depart from these specific details. Details of well known methods, devices, and circuits are omitted so as not to obscure the description of the invention.

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According to an exemplary embodiment, the dynamic range of a receiver is maximized in the presence of a narrowband interfering signal by adjusting a third order input intercept point of a low noise amplifier in the receiver depending on a computed error rate of a received signal.

5           FIG. 3 illustrates a receiver path according to an exemplary embodiment of the present invention. For simplicity of illustration, a transmitting path is not shown in FIG. 3. It will be appreciated that the receiver path of FIG. 3 can be used in conjunction with any suitable transmitting path, such as the transmitting path shown in FIG. 1.

          In FIG. 3, the receiving path includes an RX LNA 155, an RX Filter 160, a  
10   Mixer 170, an IF Filter 180, and an Amplifier/Detector 190. The RX LNA 155 amplifies signals received from the Duplexor 140. The RX Filter 160 filters the amplified signals to remove noise and suppress spurious effects, the Mixer 170 mixes the filtered signals with a local oscillator frequency, the IF Filter 180 filters the signals to an intermediate frequency, and the Amplifier/Detector 190 amplifies and detects the filtered  
15   signals, producing digital baseband data which is processed by the DSP 200.

          According to an exemplary embodiment, the third order input intercept point and the gain of the RX LNA 155 are adjustable, depending on the state of operation of the transceiver, to maximize the dynamic range of the receiver.

          The third order input intercept point of the RX LNA 155 may be selected based  
20   on several factors, e.g., the transmit power level of the system, the received signal strength, etc. According to an exemplary embodiment, the transmit power level is used to adjust the third order intercept point. The transmit power level may be detected in any conventional manner, e.g., by direct measurement of the transmit signal, through inference based on the detected received signal strength, or by referring to a look-up table  
25   in the DSP 200. To avoid the problems associated with the prior art, an error rate, such as a bit error rate or frame erasure rate (FER), of the received signal may also be used in the selection of the third input intercept point. For this purpose, the DSP 200 processes the digital baseband data output from the Amplifier/Detector 190 and determines the FER



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from the checksum within each frame of the digital data in a conventional manner. The DSP 200 may be implemented as, e.g., a programmable microprocessor.

A transceiver according to the IS-95 standard dynamically varies the transmitter power level over approximately an 80 dB range. The DSP 200 determines whether the detected transmit power level is high or low. If the transmit power level is high, e.g., within 10 dB of the upper limit of the transmit power range, the third order intercept point is set to a maximum level. If the transmit power level is low, e.g., more than 10 dBm below maximum power, the DSP 200 determines whether the FER exceeds a predetermined threshold, e.g.,  $\frac{1}{2}$  %. According to an exemplary embodiment, if the FER exceeds the predetermined threshold and the transmit power level is low, the third order input intercept point of the LNA 155 is set to a maximum level. If the transmit power level is low but the FER does not exceed the predetermined threshold, the third order input intercept point is set to a minimum level. In this manner, the dynamic range of the receiver is improved in the presence of a narrowband interfering signal, and current is saved in the receiver.

The gain of the RX LNA 155 may also be selected based on the received signal strength. According to an exemplary embodiment, the received signal strength may be detected in a conventional manner by, e.g., the DSP 200.

The DSP 200 determines whether the detected signal strength exceeds a predetermined threshold. If the received signal strength is below a predetermined threshold, e.g., less than 30 dB above the receiver sensitivity, the gain of the RX LNA 155 is set to a maximum level. If the received signal strength is above the predetermined threshold, e.g., greater than 30 dB above the receiver sensitivity, the gain is set to a minimum level. The DSP 200 adjusts the gain and third order input intercept point of the LNA 155 by transmitting appropriate control signals via, e.g., control lines 210 and 220. Although two control lines are shown in FIG. 3 for illustrative purposes, it will be appreciated that a single control line or more than two control lines may be used for this purpose. The control signals trigger adjustment of the gain and third order input intercept point via, for example, a transistor switch and/or logic in the LNA 155.

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The selection of the third order input intercept point and the gain of the LNA 155 varies, depending on the state of operation of the transceiver. The states of operation of the transceiver may be categorized as follows:

5	<u>State 1</u>	<u>State 2</u>
	TX operates at high power	TX operates at reduced power
	RX signal strength below threshold	RX signal strength below threshold
	FER not used	FER below threshold
10	LNA gain maximum	LNA gain maximum
	LNA input intercept point maximum	LNA input intercept point minimum
15	<u>State 3</u>	<u>State 4</u>
	TX operates at reduced power	TX operates at reduced power
	RX signal strength above threshold	RX signal strength above threshold
	FER below threshold	FER above threshold
20	LNA gain minimum	LNA gain minimum
	LNA input intercept point minimum	LNA input intercept point maximum

State 1 refers to a situation in which the subscriber unit is located, e.g., a long  
25 distance from the CDMA base station. In this situation, the transmit power level is high so the LNA third order input intercept point is set at a maximum level, without having to consider the FER rate. Also, the RX signal strength is below the threshold, so the LNA gain is set to a maximum level.

State 2 refers to a situation in which the subscriber unit is, e.g., closer to the  
30 CDMA base station. In this situation, the transmit power is low, but the FER is still within acceptable limits, so the LNA third order input intercept point is set at a minimum level. Also, the RX signal strength is below the threshold, so the LNA gain is set to a maximum level.

The FER may increase during State 2, e.g., if the subscriber unit moves close to  
35 an AMPS telephone or AMPS microcell. If the FER increases to the point of exceeding

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the threshold during State 2, the LNA third order input intercept point is adjusted to the maximum level.

State 3 refers to a situation in which the subscriber unit is, e.g., even closer to the CDMA base station. As in State 2, the transmit power level is low, but the FER is still  
5 within acceptable limits, so the LNA third order input intercept point is set at a *minimum* level. However, the RX signal strength is above the threshold, so the LNA gain is set to a minimum level.

As in State 2, the FER may increase during State 3 to such a point that it exceeds the threshold. In this case, the LNA third order input intercept point is adjusted to the  
10 maximum level.

State 4 refers to a situation in which the subscriber unit is close to a narrowband base station, e.g., an AMPS base station. In this situation, as in State 3, the RX signal strength is above the threshold, so the LNA gain is set to a minimum level. However, the transmit power level is low, and the FER exceeds the threshold, so the LNA third  
15 order input intercept point is set at a maximum level.

According to the present invention, the third order input intercept point of the LNA is increased, in response to an increased FER rate and a reduced transmit power level, to extend the dynamic range of the receiver. Because the undesired TX crossmodulation products vary inversely as the square of the LNA third order input  
20 intercept point, a small increase in the third order input intercept point results in a larger decrease in the TX crossmodulation products. For example, a 1 dB increase in the third order input intercept point results in a 2 dB decrease in the TX crossmodulation products. Thus, by increasing the LNA third order input intercept point in response to an FER above a predetermined threshold and a low transmit power level, the level of interfering  
25 signal required to degrade the FER is effectively increased, thus optimizing the dynamic range for handling the interfering signal.

FIG. 4 illustrates a method for improving the dynamic range of a receiver, according to an exemplary embodiment of the present invention. The method begins at

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step 400, at which the received signal strength and the transmit power level of the received signal are detected.

At step 410, a determination is made by the DSP 200 whether the received signal strength is below a predetermined threshold. If the received signal strength is below a  
5 predetermined threshold, the gain of the LNA 155 is set at a maximum level at step 420. If the received signal strength is not below a predetermined threshold, the gain of the LNA 155 is set at a minimum level at step 430.

At step 440, a determination is made by the DSP 200 whether the transmit power level is high. If the transmit power level is high, the third order input intercept point of  
10 the LNA 155 is set at a maximum level at step 470. If the transmit power level is not high, the FER is computed at step 450.

From step 450, the DSP 200 determines whether the FER is greater than a predetermined threshold, e.g.,  $\frac{1}{2}$  %. If the FER is greater than the predetermined threshold, the third order input intercept point is set to a maximum level at step 470. If  
15 the FER does not exceed the predetermined threshold, the third order input intercept point is set to a minimum level at step 480. It will be appreciated that the order of the steps 410-430 and steps 440-480 may be interchanged, i.e., the gain may be adjusted before, after, or at the same time as the third order input intercept point.

FIGS. 5A-5D illustrate simulations of a system according to the present invention,  
20 in various states of operation. Typical parameters for IS-95 CDMA filters and gain stages were used in the simulations. In addition, the system bandwidth was set at 1250 Kilo Hertz (KHz), the Energy per bit to noise ratio (Eb/No) was set at 4.5 dB, the processing gain was set at 21.07 dB, and the traffic channel offset was set at -15.60 dB.

In FIG. 5A, which represents State 1, the transmitter was operating at high  
25 power, and the received signal strength was below the threshold. In this state, the LNA gain was set to a maximum level of 15 dB, and the LNA third order input intercept point was set to a maximum of 15 dB. As can be seen from FIG. 5A, under these conditions, the Receiver Noise Figure (NF) was 7.26 dB, the Receiver Input Intercept Point (IPi) was -5 dBm, the Sensitivity of the receiver was -106.32 dBm, and the Receiver Gain was

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62.2 dB.

In FIG. 5B, which represents a simulation of State 2, the transmit power level was low, and the received signal strength was below the threshold. In this state, the LNA third order input intercept point was reduced by 10 dB to a minimum level of 5 dB, but the LNA gain remained at the maximum level. As can be seen from FIG. 5B, there was minimal change in the receiver's overall system performance from State 1, with the only change being a reduction in the Receiver IPi to -5.13 dBm.

In FIG. 5C, which represents a simulation of State 3, the transmit power level was low, and the received signal strength was above the threshold. The gain of the LNA 155 was reduced by -20 dB to -5 dB, but the LNA third order input intercept point remained at the minimum level. As can be seen from FIG. 5C, reducing the gain of the LNA 155 improved the overall system input intercept point in spite of the LNA 155 operating at a reduced third order input intercept point. In addition, an LNA NF increase from 2 dB to 22 dB was factored in, as result of reducing the LNA gain. Under these conditions, the system NF increased from 7.65 dB to 27.6 dB, the Receiver IPi increased to 8.65 dBm, the Receiver Sensitivity decreased to -86.323 dBm, and the Receiver Gain decreased to 42.2 dB.

In FIG. 5D, which represents a simulation of State 4, the transmit power level was low, and the received signal strength was above the threshold. The gain of the LNA 155 remained at the minimum level, but the LNA third order input intercept point was increased by 10 dB to 15 dB, in response to an FER exceeding the threshold. As can be seen from FIG. 5D, system performance remained the same as in State 3, except that the Receiver IPi increased from 8.65 dBm to 13.7 dBm. In actual operation, this increase in the receiver input intercept point translates into an improvement in strong handling capacity. Also, assuming that the RX Filter 160 is sufficient to prevent any significant crossmodulation from the Mixer 170, a 10 dB increase in the LNA third order input intercept point corresponds to a 20 dB reduction in the undesired crossmodulation product, effectively increasing the dynamic range of the receiver to this type of interference.

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It will be understood that the invention is not limited to the particular embodiments that are described and illustrated above. For example, although the embodiment described above is directed to a CDMA cellular telephone network, the invention is also be applicable to other types of radio telephone systems. The  
5 specification contemplates any and all modifications that fall within the scope of the invention as defined by the following claims.

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**WHAT IS CLAIMED IS:**

1. An apparatus for improving the dynamic range of a receiver, comprising:  
a processor for computing an error rate of a received signal; and  
5 a low noise amplifier with an adjustable input intercept point, wherein the input intercept point is adjusted depending on the computed error rate.
2. The apparatus of claim 1, wherein the input intercept point is adjusted  
based also on a transmit power level.  
10
3. The apparatus of claim 2, wherein if the transmit power level is low, and  
the computed error rate exceeds a predetermined threshold, the input intercept point is set  
at a maximum level.
- 15 4. The apparatus of claim 2, wherein if the transmit power level is low, and  
the computed error rate does not exceed a predetermined threshold, the input intercept  
point is set at a minimum level.
- 20 5. The apparatus of claim 2, wherein if the transmit power level is high, the  
input intercept point is set at a maximum level.
6. The apparatus of claim 1, wherein the computed error rate is a frame  
erasure rate.
- 25 7. The apparatus of claim 1, wherein a gain of the low noise amplifier is  
adjusted based on a received signal strength.
8. A system for receiving and transmitting signals, comprising:  
a transmitting path for processing signals for transmission; and

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a receiving path for processing received signals, the receiving path including a low noise amplifier with an adjustable input intercept point and a processor for computing an error rate of a received signal, wherein the input intercept point is adjusted depending on the computed error rate.

5

9. The system of claim 8, wherein the input intercept point is also adjusted depending on a transmit power level of the system.

10. The system of claim 9, wherein if the transmit power level is low, and the computed error rate exceeds a predetermined threshold, the input intercept point is set at a maximum level.

11. The system of claim 9, wherein if the transmit power level is low, and the computed error rate does not exceed a predetermined threshold, the input intercept point is set at a minimum level.

12. The system of claim 9, wherein if the transmit power level is high, the input intercept point is set at a maximum level.

13. The system of claim 8, wherein the computed error rate is a frame erasure rate.

14. The system of claim 8, wherein a gain of the low noise amplifier is adjusted based on a received signal strength.

25

15. A method for improving the dynamic range of a receiver, the method comprising the steps of:

computing an error rate of a received signal; and



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adjusting an input intercept point of a low noise amplifier in the receiver,  
depending on the computed error rate.

16. The method of claim 15, further comprising a step of detecting a transmit  
5 power level, wherein the input intercept point is selected based also on the detected  
transmit power level.

17. The method of claim 16, wherein if the detected transmit power level is  
low, and the computed error rate exceeds a predetermined level, the input intercept point  
10 is set at a maximum level.

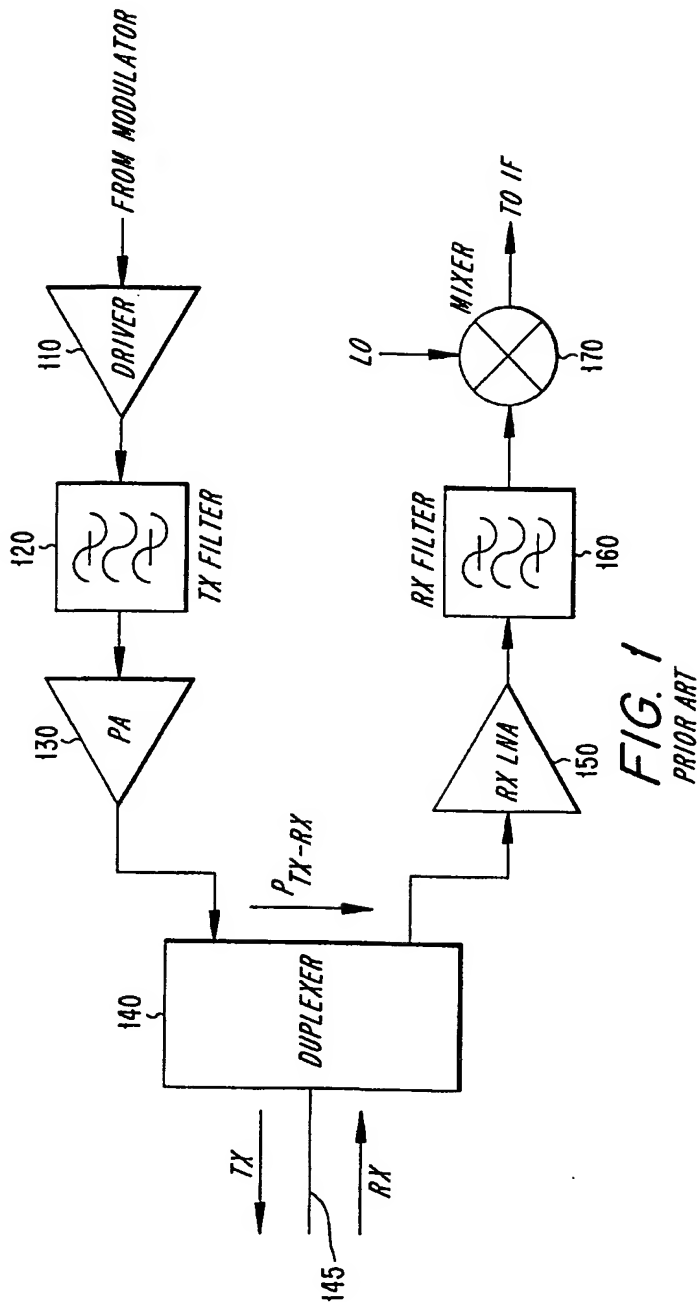
18. The method of claim 16, wherein if the transmit power level is low, and  
the computed error rate does not exceed a predetermined threshold, the input intercept  
point is set at a minimum level.

15

19. The method of claim 16, wherein if the transmit power level is high, the  
input intercept point is set at a maximum level.

20. The method of claim 15, wherein the computed error rate is a frame  
20 erasure rate.

21. The method of claim 15, further comprising the steps of:  
detecting a received signal strength; and  
selecting a gain of the low noise amplifier based on the detected received  
25 signal strength.



TX MODULATION

FIG. 2A

PRIOR ART

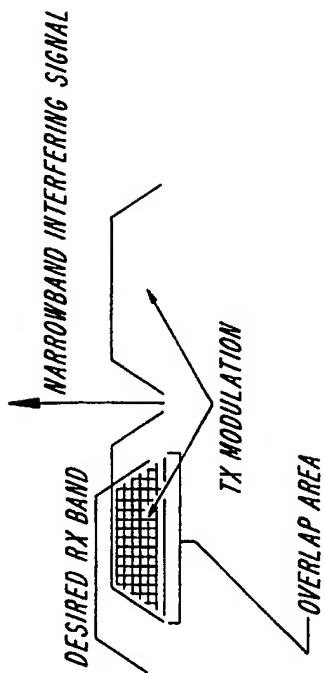


FIG. 2B  
PRIOR ART

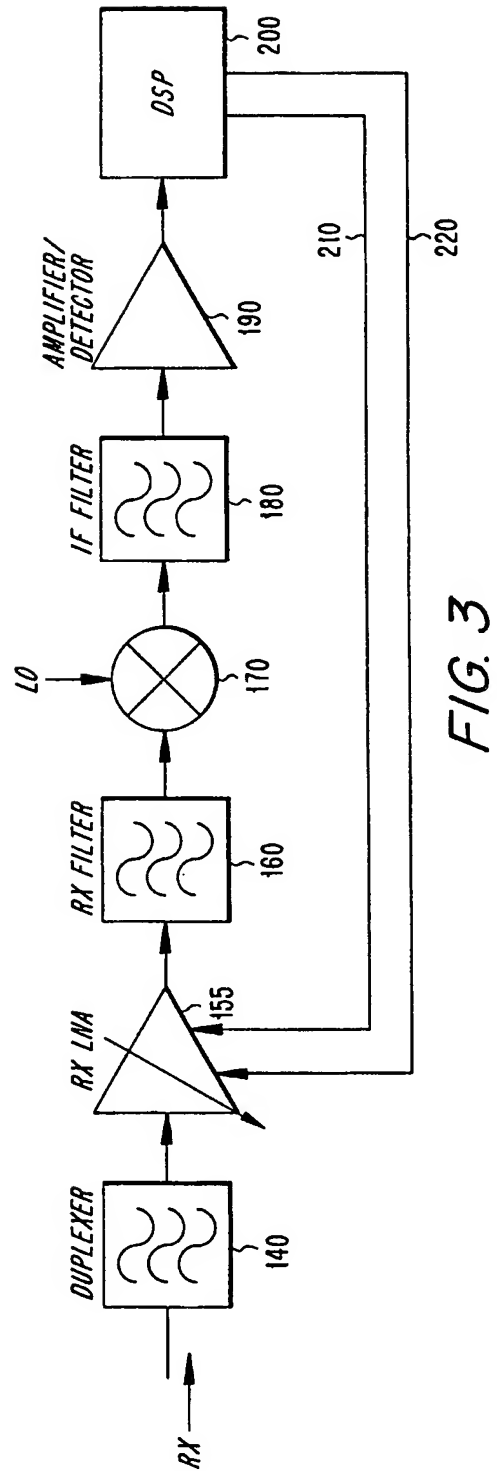
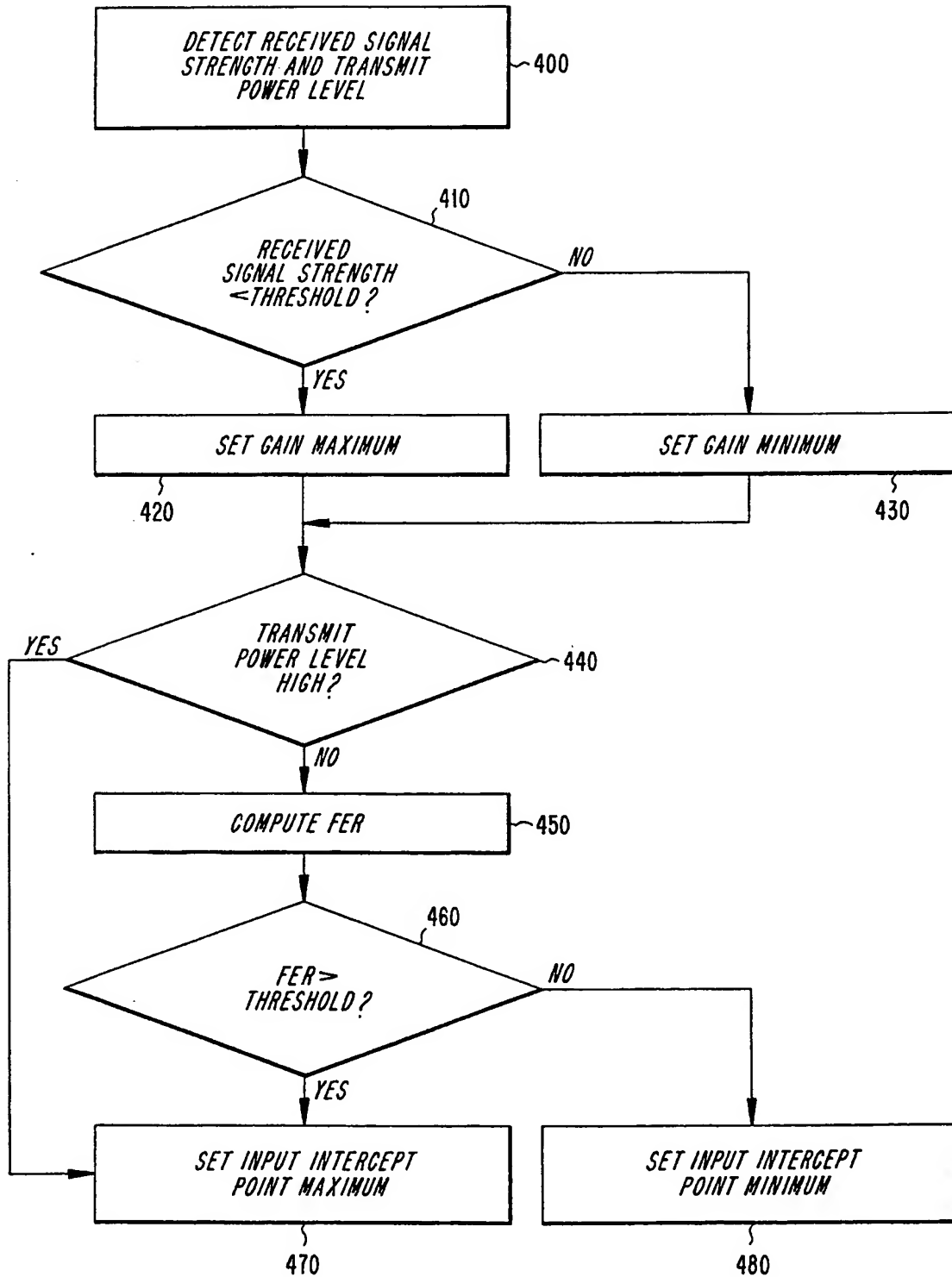


FIG. 3

3/7

FIG. 4



CDMA Receiver System Calculator									
File									
<div style="display: flex; justify-content: space-between;"> <div> <p>Title:</p> <p>Typical IS-95 CDMA Receiver, Operational State 1</p> </div> <div> <p>Version 1.10</p> </div> </div>									
G @ f0 in dB	-4.8	15	-3	15	-10	50			
G @ f1 in dB	-4.8	15	-3	15	-45	50			
G @ f2 in dB	-4.8	15	-3	15	-50	50			
IPi in dBm	100	15	100	3	100	-40			
NF in dB	4.8	2	3	7	10	5			
<div style="display: flex; justify-content: space-between;"> <div style="width: 30%;"> <p>Amplifier</p> <p>Attenuator</p> <p>Filter</p> <p>Mixer</p> <p>Delete</p> </div> <div style="width: 40%;"> <p>System BW (kHz)</p> <p>Eb/No Required (dB)</p> <p>Processing Gain (dB)</p> <p>Traffic Ch. Offset (dB)</p> </div> <div style="width: 25%;"> <p>1250</p> <p>4.5</p> <p>21.07</p> <p>-15.60</p> </div> </div>									
<div style="display: flex; justify-content: space-around;"> <div>Calculate</div> <div>Print</div> </div>									
<div style="border: 1px solid black; padding: 5px;"> <p>Calculated System Parameters</p> <p>System NF = 7.65 dB</p> <p>System IPi = -5.00 dBm</p> <p>Sensitivity = -106.32 dBm</p> <p>System Gain = 62.2 dB</p> </div>									

FIG. 5A

CDMA Receiver System Calculator

---

File

Version 1.10

---

Title:

Typical IS-95 CDMA Receiver, Operational State 2

	Duplexor	RX LNA	RX Filter	Mixer	IF Filter	
G @ f0 in dB	-4.8	15	-3	15	-10	50
G @ f1 in dB	-4.8	15	-3	15	-45	50
G @ f2 in dB	-4.8	15	-3	15	-50	50
IPi in dBm	100	5	100	3	100	-40
NF in dB	4.8	2	3	7	10	5

Amplifier

Attenuator

Filter

Mixer

Delete

System BW (kHz)

Eb/No Required (dB)

Processing Gain (dB)

Traffic Ch. Offset (dB)

Calculate

Print

Calculated System Parameters

System NF = 7.65 dB

System IPi = -5.13 dBm

Sensitivity = -106.32 dBm

System Gain = 62.2 dB

FIG. 5B

CDMA Receiver System Calculator

File

Version 1.10

Title

Typical IS-95 CDMA Receiver, Operational State 3

Duplexor

RX LNA

RX Filter

Mixer

IF Filter

G @ f0 in dB	-4.8	-5	-3	15	-10	50
G @ f1 in dB	-4.8	-5	-3	15	-45	50
G @ f2 in dB	-4.8	-5	-3	15	-50	50
IPi in dBm	100	5	100	3	100	-40
NF in dB	4.8	22	3	7	10	5

Calculated System Parameters

System NF = 27.6 dB

System IPi = 8.65 dBm

Sensitivity = -86.323 dBm

System Gain = 42.2 dB

System BW (kHz)

1250

Eb/No Required (dB)

4.5

Processing Gain (dB)

21.07

Traffic Ch. Offset (dB)

-15.60

Amplifier

Attenuator

Filter

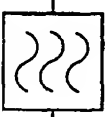
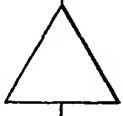
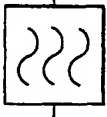
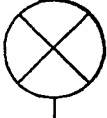
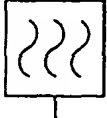
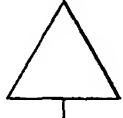
Mixer

Delete

Calculate

Print

FIG. 5C

CDMA Receiver System Calculator									
File									
<div style="display: flex; justify-content: space-between;"> <div> <p>Title</p> <p>Typical IS-95 CDMA Receiver, Operational State 4</p> </div> <div> <p>Version 1.10</p> </div> </div>									
<div style="display: flex; justify-content: space-around; align-items: center;"> <div style="text-align: center;"> <p>Duplexor</p>  </div> <div style="text-align: center;"> <p>RX LNA</p>  </div> <div style="text-align: center;"> <p>RX Filter</p>  </div> <div style="text-align: center;"> <p>Mixer</p>  </div> <div style="text-align: center;"> <p>IF Filter</p>  </div> <div style="text-align: center;">  </div> </div>									
G @ f0 in dB	-4.8	-3	-5	15	-10	50			
G @ f1 in dB	-4.8	-3	-5	15	-45	50			
G @ f2 in dB	-4.8	-3	-5	15	-50	50			
IPi in dBm	100	100	15	3	100	-40			
NF in dB	4.8	3	22	7	10	5			

Amplifier

Attenuator

Filter

Mixer

Delete

System BW (kHz)

1250

Eb/No Required (dB)

4.5

Processing Gain (dB)

21.07

Traffic Ch. Offset (dB)

-15.60

Calculate

Print

Calculated System Parameters

System NF = 27.6 dB

System IPi = 13.7 dBm

Sensitivity = -86.323 dBm

System Gain = 42.2 dB

FIG. 5D



# INTERNATIONAL SEARCH REPORT

In national Application No

PCT/US 99/04783

**A. CLASSIFICATION OF SUBJECT MATTER**  
IPC 6 H04B1/10

According to International Patent Classification (IPC) or to both national classification and IPC

**B. FIELDS SEARCHED**

Minimum documentation searched (classification system followed by classification symbols)

IPC 6 H04B

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

**C. DOCUMENTS CONSIDERED TO BE RELEVANT**

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X A	US 5 697 081 A (LYALL JR ROBERT L ET AL) 9 December 1997 see abstract; figure 1  see column 2, line 20 - column 3, line 60 -----	1,7,8, 14,15,21 2-6, 9-13, 16-20
A	US 5 359 607 A (NGUYEN TUAN K ET AL) 25 October 1994 see abstract; figure 2 see column 1, line 11 - column 2, line 28 -----	1-21

☐ Further documents are listed in the continuation of box C.

☒ Patent family members are listed in annex.

\* Special categories of cited documents :

"A" document defining the general state of the art which is not considered to be of particular relevance

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"L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)

"O" document referring to an oral disclosure, use, exhibition or other means

"P" document published prior to the international filing date but later than the priority date claimed

"T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention

"X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone

"Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art.

"&" document member of the same patent family

Date of the actual completion of the international search

30 June 1999

Date of mailing of the international search report

06/07/1999

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Authorized officer

Andersen, J.G.

# INTERNATIONAL SEARCH REPORT

Information on patent family members

International Application No

PCT/US 99/04783

Patent document cited in search report	Publication date	Patent family member(s)	Publication date
US 5697081 A	09-12-1997	AU 6974196 A WO 9710649 A	01-04-1997 20-03-1997
US 5359607 A	25-10-1994	JP 2868961 B JP 5259929 A	10-03-1999 08-10-1993